



COPY OF PAPERS  
ORIGINALLY FILED

Express Mail No. EM401141116US

Patent Application  
Attorney Docket DVS-007

## High Power Modulator

### Field of the Invention

5 This invention relates to the field of high voltage modulators and, more particularly, to solid state~~X~~ modulators for high voltage systems.

### Background

RECEIVED

JUL 23 2002

TECHNOLOGY CENTER 2800

Reliable high-speed, high-power switching has a wide variety of applications such as radar and communications transmitters, ion implantation, particle accelerators,  
10 induction heating, and materials processing. Applications of high-speed, high-power switching require consistent, controllable, rapid, and cost-effective switching of high levels of electrical power. The components and technologies currently available to support these high-power switching applications were developed in the 1930's and 1940's. Despite the revolution in cost and performance that solid state technology has  
15 brought to nearly every other realm of electronics, progress with solid state high voltage and high power switching devices has been slow and improvements have been modest.

For example, vacuum switch tubes or thyratrons, alone or in combination with Pulse Forming Networks (PFNs) and pulse transformers, have been used to switch high voltage power supplies and high voltage loads, such as gyroklystrons. The non-ideal  
20 behavior of tube switches, however, results in numerous undesirable characteristics, such as large effective on-voltage drop, limited current capability and speed, limited Pulse

drives within the device itself, which were required because of the low betas of prior art high-current bipolar circuit designs.

IGBTs can be used for high voltage switching by connecting many devices in series. This technique is described in, for example, U.S. Patent No. 5,444,610 (hereinafter "the '610 patent"), which is assigned to the assignee of the present application, and which is incorporated herein by reference. The '610 patent describes a high power modulator capable of switching high voltages using large numbers of low voltage switches connected in series, where each of the switches is connected in parallel with a voltage limiting means. This technique provides the flexibility of a modular design with no inherent limit to voltage handling, because the voltage limiting means described in this patent has virtually unlimited voltage and current carrying capability.

For some applications, however, the apparatus described in the '610 patent may be physically large and expensive to manufacture. For example, to switch 120 kV, up to 160 series connected IGBTs may be required, which presents size and configuration challenges. In addition, so that no single IGBT sees harmful or destructive voltages, the load must be shared equally among <sup>the</sup> each IGBT device<sup>s</sup>. Therefore, the gate drives for the IGBT devices must be <sup>precisely</sup> ~~highly~~ synchronized.

Thus, an object of the present invention is to incorporate serially connected low voltage switches having load sharing features in a compact, transformer coupled gate switch. By floating each IGBT and its respective gate drive circuitry with respect to ground, ~~and~~ by ensuring that all power and control connections to the IGBT and its gate drive are isolated, <sup>and voltage limiting means are provided</sup> no single IGBT will experience a voltage greater than its design limit.

In addition, the IGBT devices can be highly synchronized and, therefore, can switch substantially simultaneously.

Thus, the present invention features a modulator that comprises one or more transformers and a plurality of switches. The transformers comprise a primary and a plurality of secondary windings. Each secondary winding has an output terminal pair. Each of the plurality of switches is associated with a respective secondary winding and has <sup>an output-high terminal and an output-low terminal</sup> ~~input and output terminals~~ and a control terminal. The control terminal <sup>pair</sup> of each switch is in electrical communication with a respective output terminal <sup>pair</sup> of the plurality of secondary windings. When an input signal is applied to the primary of the transformer, a signal is induced in the secondary such that the plurality of switches, which are each coupled to a respective secondary winding, are switched substantially simultaneously.

In one embodiment, the modulator further comprises a stack of <sup>switch modules</sup> ~~modulators~~ sharing the same primary <sup>as shown in Figs. 5 and 6</sup>. In other embodiments, the modulator further comprises at least one voltage limiter, such as a Zener diode or snubbing circuit, and in one embodiment the at least one voltage limiter is connected in parallel with <sup>the output terminal pair of</sup> at least one of the plurality of switches. In another embodiment, the plurality of switches are connected in series or in parallel <sup>to better match the properties</sup> ~~according to the configuration~~ of the load. In further embodiments, at least one of the plurality of switches comprises a transistor, such as an insulated gate bipolar transistor (IGBT), an avalanche-rated field effect transistor (FET), or a power metal oxide FET (MOSFET).

The present invention also features a modulator comprising a transformer, a plurality of retriggerable drive circuits, and a plurality of switches <sup>as shown in Figs. 7 and 8</sup>. The transformer

includes a primary and a plurality of secondary windings. Each of the plurality of retriggerable drive circuits has an output<sup>terminal pair</sup> and is electrically connected to a respective one of the plurality of secondary windings. Each of the plurality of switches is associated with a respective retriggerable drive circuit and has ~~two~~<sup>an</sup> output terminal<sup>pair</sup> and a control terminal<sup>pair</sup>. The control terminal<sup>pair</sup> of each switch is in electrical communication with a respective output terminal<sup>pair</sup> of the retriggerable drive circuit with which it is associated. In one embodiment of the invention, the modulator comprises a stack of ~~modulators~~<sup>switch modules</sup> sharing the primary of the transformer<sup>s</sup>. In operation, when an input signal is applied to the primary of the transformer<sup>s</sup>, each of the plurality of switches is switched substantially simultaneously and remains substantially on until a second signal is applied to the primary of the transformer to turn the switches off.

The present invention also features a method of switching a signal. An input signal is applied to the primary of a transformer. In response to this input signal, a voltage is induced in a plurality of secondary windings of the transformer. This induced voltage switches, substantially simultaneously, each of a plurality of switches that are electrically controlled by a respective one of the plurality of secondary windings. In one embodiment of the invention, each of the plurality of switches is maintained in a substantially conducting state after termination of the input<sup>trigger</sup> signal. In another embodiment, a ~~reset input signal~~<sup>gate trigger pulse</sup> is applied to the single primary winding of the transformer.

The present invention also features a modulator that may be used as a very large, very fast series switch, or circuit breaker that enables high power systems to be turned on

and off in a rapid, repeatable, and controllable way. When the modulator is used as a switch, power can be substantially removed from the load when the switch is 'off', ~~or~~ *that is* open.

The foregoing and other objects, aspects, features, and advantages of the invention will become more apparent from the following description and from the claims, when viewed in conjunction with the accompanying drawings.

#### Brief Description of the Drawings

Fig. 1 is a simplified schematic diagram of a modulator with switches connected in series, in accordance with one embodiment of the invention.

Fig. 2 is a simplified schematic diagram of a modulator with switches connected in series that includes voltage limiting means, in accordance with the invention.

Fig. 3 is a simplified schematic of one embodiment of a modulator with series connected switches, in accordance with the invention.

Fig. 4 is a simplified schematic diagram of a modulator having switches connected in parallel, in accordance with an embodiment of the invention.

Fig. 5 is a three dimensional diagram of one embodiment of the ~~modulator~~ <sup>switch modules</sup> of the present invention.

Fig. 6 is a simplified schematic of a modulator that includes stacked ~~modulators~~ <sup>switch modules</sup>, in accordance with the invention.

Fig. 7 is a simplified schematic of a retriggerable modulator, in accordance with an embodiment of the invention.

Fig. 8 is a simplified schematic of another implementation of a retriggerable modulator, in accordance with an embodiment of the invention.

## 5 Detailed Description

Modulators are electronic devices used to precisely regulate the delivery of high voltage, high current electrical pulses. A modulator can act as a simple <sup>series</sup> switch between a high power supply and its load (such as a klystron). Ideally, modulators have infinite voltage holdoff, infinite off-resistance, zero on-resistance, and full immunity to transients and voltage reversals. Modulators are critical components of electronic systems used for numerous applications such as radar systems, particle accelerators, medical diagnostics and treatment equipment, and manufacturing equipment, such as ion implantation for semiconductor fabrication. In addition, new processes for food sterilization, waste treatment, and pollution control are also being developed which require the use of high power modulators.

Many high power modulators use pulse transformers to allow switching of the required pulse energy at low voltage. However, conventional pulse modulators generally require large subsystems and vacuum tubes, alone or in combination with pulse-forming networks (PFN's) to drive the pulse transformer. A pulse forming network (PFN) modulator is an electronic device used to precisely regulate the delivery of high voltage, high current electrical pulses.

Achieving a nearly ideal pulse is critical to the performance of a number of pulsed power applications. An "ideal pulse" has instantaneous rise and fall time and a flat top, independent of load current and repetition rate. In ion implantation applications, for example, it is critical to minimize the voltage drop and pulse-to-pulse voltage variation to achieve uniform <sup>doping</sup> ~~processing~~. This requires very fast rise and fall times to minimize the energy provided at voltages other than the amplitude of the pulse. It also requires a very flat-top for the pulse, with no ripple or droop. In radar applications, the rise and fall times must be within the amplifiers' operating parameters. The flat top is very critical to parameters such as phase noise. Generating pulses that most closely approach the ideal pulse waveform is, therefore, often a critical objective of high pulsed power system design.

Historically, vacuum switch tubes or thyratrons, alone, or in combination with PFNs and pulse transformers, have been used to generate pulse waveforms. These conventional switches have non-ideal behavior, such as a large effective voltage drop, limited current capability and speed, high maintenance, and complex driving and protection circuitry. Nevertheless, they have ~~provided a nearly exclusive solution to the~~ <sup>dominated</sup> ~~problem of~~ high-voltage switching until recently because no cost effective alternatives <sup>have been</sup> ~~were~~ available. As future system requirements extend to higher voltage and power, however, the use of switch tubes becomes increasingly impractical due to the inherent voltage and current limits of these devices.

The physical size of prior art power modulator systems, moreover, generally is very large, which is problematic for many applications. Furthermore, the expected

lifetime of conventional power modulator systems using vacuum tubes and pulse forming networks is generally low. To meet these and other needs, the present invention, provides a reliable, fast, compact, low-current, transformer coupled gate switch technology modulator.

5           The present invention features a solid state modulator that can be used in systems that would otherwise require a switch tube, spark gap, or thyatron pulse forming network (PFN) modulator to switch high voltage and power. Fig. 1 illustrates a modulator 10 according to the present invention that is connected between a power source 21 and a load 14. The modulator 10 includes a transformer 16 connected to the <sup>control driver</sup> ~~trigger source~~ 12, and a  
10   plurality of switches 18 connected in series. The transformer 16 further includes a primary winding 20 and a plurality of secondary windings 22. The primary winding 20 may be connected to ground potential while the plurality of secondary windings 22 may float at staggered high voltages. In one embodiment of the invention, the primary  
winding 20 further includes an input terminal <sup>pair</sup> and each secondary winding 22 further  
15   includes an output terminal <sup>pair</sup>.

In addition, although the primary winding 20 is illustrated in Fig. 1 as a single winding, in other embodiments of the invention, the primary winding 20 is a plurality of <sup>turns</sup> ~~windings~~ that achieve a predetermined turns ratio (i.e. 2:1 or 4:1). In another  
embodiment, the primary winding 20 may be a portion of a winding such as a half-turn of  
20   a winding. In another embodiment the primary winding 20 is a distributed primary winding. Distributing the winding can improve geometrical packing and reduce leakage inductance.



The transformer 16 can be formed using a toroidal core comprising a high permeability material such as ferrite. Using a toroid provides the advantage that the length <sup>and conformation</sup> of wire forming each secondary winding 22 will be <sup>essentially</sup> the same, so that the switches 18 will turn off and on at the same time. In another embodiment (as described in connection with Fig. 6), the modulator 10 includes one or more <sup>switch modules</sup> ~~modulators~~ stacked together, with the transformer 16 of each <sup>switch modules</sup> ~~modulator~~ sharing the same primary winding 20. In one embodiment, the stacked modulator configuration comprises stacks of toroids forming the transformers 16 of the modulators. <sup>Closely stacking</sup> ~~Stacking~~ the toroids is advantageous because it helps to reduce leakage inductance <sup>and enables building modules at very high voltage.</sup>

Each switch 18 is associated with a respective secondary winding 22. In one embodiment (not shown), each switch is electrically coupled to a respective output terminal <sup>pair</sup> of the respective secondary winding 22. Each switch 18 includes a transistor, such as an insulated gate bipolar transistor (IGBT), an avalanche FET, or a power MOSFET. For example, a modulator 10 may include an arbitrary number of switches 18, such as IGBTs, connected in parallel and/or in series (which is explained further below). In one embodiment, the switches 18 include a combination of different types of switches,

such as a combination of IGBTs and avalanche FETs. In one embodiment, each switch 18 includes <sup>an output</sup> ~~a~~ voltage limiting means. <sup>input voltage limiting means and an output voltage limiting means, such as disclosed in the '610 patent.</sup> In another embodiment, each switch 18 includes an

Power MOSFETs, unlike conventional bipolar transistors, are essentially voltage driven devices. Moreover, because power MOSFETs are majority carrier devices and have minimal minority carrier storage time, power MOSFETs have exceptionally fast

rise/fall times. Power MOSFETs also are rugged-switching devices because they lack the secondary breakdown effect of bipolar transistors.

In comparison, IGBTs have the high input impedance and high speed characteristics of a MOSFET with the conductivity characteristics of a bipolar transistor.

5 In addition, IGBTs can be turned on and turned off electronically, in contrast to thyristor switches conventionally used in some power modulators, which can only be turned on electronically. The fact that IGBT and MOSFET switches turn off electronically with low-power <sup>control</sup> pulses eliminates the need for PFNs in the modulator.

IGBT switches may be characterized by a low voltage drop <sup>in their on-state</sup> for example about 2.5  
10 Volts, so that in saturation the IGBT is essentially a Darlington pair configuration with a FET as the input stage and a bipolar power transistor for the output stage. The risetime of IGBTs is largely determined by the gate drive circuitry, as described below.

In another embodiment, each switch 18 includes avalanche FETs, such as a thousand volt FET with an avalanche rating. A typical avalanche FET could have a  
15 saturated on-state resistance of  $2\Omega$  and a switching time of about 30 nsec, both of which are sufficient for the modulator applications described herein.

When the switches 18 are connected in series, as illustrated in Fig. 1, each individual series connected switch 18 operates with a floating ground reference. Consequently, all switches will perform identically and none should experience any  
20 voltage greater than its design limits regardless of the end of the series stack at which it is located. Each switch 18 and its gate drive circuitry (not shown) can "float" relative to

ground, and all <sup>enabling</sup> ~~power~~ and control connections to the switches 18 may be made

inductively. Thus, in the embodiment illustrated in Fig. 1, a trigger can be applied at the

input <sup>9</sup> ~~12~~ and <sup>enabling</sup> ~~power~~ 21 <sup>to</sup> ~~can~~ be applied to <sup>load via switches</sup> ~~the switch~~ 18. In response to the <sup>control signal applied to</sup> ~~power applied~~

~~and a trigger at~~ the primary, a voltage is induced at each secondary 22 of the transformer

5 at substantially the same time. Thus, <sup>switches</sup> ~~each switch~~ 18 will be switched substantially simultaneously.

In one embodiment, the switch 18 is an IGBT, the FET inputs (i.e., the gate signals) are electrically coupled in parallel to the transformer 16 and the outputs of each switch 18 are connected in series ~~or in parallel~~ <sup>20</sup> with the load 14. The primary winding ~~16~~ of the transformer is at ground potential and the secondary windings 22 are floating at staggered high voltages. For a typical IGBT switch, the gate capacitance for each IGBT is approximately 5 nF. During operation, the entire modulator 10 acts as a high voltage switch, so that when an input signal is applied <sup>to control driver</sup> ~~at trigger~~ 12 and power 21 is applied ~~to~~ the switches 18 are switched substantially simultaneously. Because the switches are in series,

10 of the transformer is at ground potential and the secondary windings 22 are floating at staggered high voltages. For a typical IGBT switch, the gate capacitance for each IGBT is approximately 5 nF. During operation, the entire modulator 10 acts as a high voltage switch, so that when an input signal is applied <sup>to control driver</sup> ~~at trigger~~ 12 and power 21 is applied ~~to~~ the switches 18 are switched substantially simultaneously. Because the switches are in series,

15 very high voltages can be switched. For example, if switch 18 is a 1200V IGBT switch and three windings are used as shown in Fig. 1, the circuit of Fig. 1 can switch 3600V by switching 1200 V across each switch 18. Additional switches can be added to switch even higher voltages.

In some embodiments of the invention, the modulator 10 can further include one or more voltage limiting devices to protect the switches 18. Fig. 2 illustrates a modulator 10 that includes a plurality of <sup>output</sup> ~~voltage~~ limiting devices 24. Each <sup>output</sup> ~~voltage~~ limiting device 24 is connected in parallel with a respective switch 18.

20

The voltage limiting device 24 is preferably integrated into the switch 18 itself.

Numerous other voltage limiting devices can also be used, such as a Zener diode, a snubbing circuit (such as described in the '610 patent), and a clamping circuit. For example, the voltage limiting means can be a metal-oxide varistor (MOV) or a capacitor connected in parallel with a series combination of a dissipating resistor and a switch (such as described in the '610 patent).

In another embodiment, the switch 18 comprises an avalanche-rated FET that has a voltage limiting capability. Regardless of the type of voltage limiting technique used, if

the voltage applied to the switch 18 is above a predetermined value, then the <sup>excess</sup> current

induced by <sup>load 14 or source 21</sup> ~~the input 12~~ will be conducted through the <sup>output</sup> voltage limiting device 24. The

corresponding voltage drop across the voltage limiting device 24, however, will be <sup>substantially</sup> independent of the current conducted therethrough

Fig. 3 illustrates a schematic diagram of one embodiment of the modulator 10, in accordance with the present invention. Eleven IGBT switches <sup>72</sup> ~~28~~ are shown to be

connected in series and are driven by parallel 1:1 windings. It should be understood, however, that the illustrations of this figure, including the windings on the transformer, are provided by way of example only. Numerous other configurations of windings can be used. For example, better geometrical packing of the windings can reduce transformer leakage. This can be accomplished by using a distributed primary winding, or by using additional windings (i.e. 2:1 or 4:1).

In addition, because leakage inductance <sup>affect the</sup> ~~impacts the induced~~ current ~~(and,~~  
~~consequently, the voltage) achievable into~~ <sup>induced in</sup> the primary, ~~the turns ratio can be adjusted for~~  
~~it may be advantageous to adjust~~

step-down operation with higher voltage primary drive. For example, a 4:2 step down can be used with a 35 V <sup>peak-to-peak</sup> drive on the transformer <sup>primary</sup>. In another example, the transformer 16 can be made from a ferrite toroid, and the ferrite toroid can be biased at the midpoint of the switches 18 ~~X~~ to reduce the maximum voltage developed between the core of transformer 16 and the switches 18.

5 In another embodiment (not shown), the transformer 16 can have multiple primary windings in parallel to improve geometrical packing (and reduce leakage inductance), ~~and through the use of much higher voltage gate drive circuitry.~~ This technique helps to overcome ~~offset the voltage-current~~ induction limitations of the leakage inductance without adding capacitance to the circuit.

10 The series connection of switches illustrated in Figs. 1, 2, and 3 provide increased voltage handling capability. <sup>In contrast</sup> Fig. 4 illustrates another embodiment of the invention wherein the switches 18 are connected in parallel, to provide increased current handling capability. In this embodiment, a control signal, such as a trigger, is applied <sup>by control driver</sup> to input 12, and this signal is coupled substantially simultaneously to each switch 18, so that the

15 switches 18 can substantially simultaneously switch current from the <sup>electrical</sup> power source ~~(current source) 21~~ ~~X~~. The ability to substantially simultaneously switch current from the power source increases the current handling capability of the modulator 10.

Fig. 5 is a three dimensional diagram <sup>representing</sup> of one embodiment of <sup>a switch module</sup> the modulator of the present invention. The <sup>switch module</sup> modulator 50 includes a transformer 16 formed of a ferrite toroid core ~~17~~ ~~X~~. As described above, using a toroid core is advantageous because the length <sup>and conformation</sup> of wire forming each secondary winding 22 can be substantially the same. This <sup>enables</sup> ~~will enable~~ each switch 18 to turn off and on at substantially the same time. Switches 18 are

positioned around the toroid core <sup>16</sup>~~17~~ and are connected to the secondary windings 22 as described above.

The <sup>switch module</sup>~~modulator~~ 50 can be surrounded by an epoxy casting 54, as illustrated in

Fig. 5. Power and load terminals 56 may be positioned at the edges of the epoxy casting

5 54. The <sup>switch module</sup>~~modulator~~ 50 of Fig. 5 is particularly suitable for stacking multiple <sup>switch modules</sup>~~modulators~~ as described below in connection with Fig. 6. Heat exchangers 52 serve to remove from the modulators heat generated in the switches 18.

Fig. 6 is a simplified schematic of a modulator 10 that includes stacked <sup>switch modules 51</sup>~~modulators~~ that share the same primary winding 20 in accordance with the invention.

Each switch 18 may include <sup>input</sup> voltage limiting means <sup>and output voltage limiting means (both not shown)</sup>~~(not shown)~~. The ability to stack <sup>switch modules</sup>~~modulators~~ and use the same primary winding to substantially simultaneously switch all switches in each of the modulators is particularly advantageous. By stacking <sup>switch modules</sup>~~modulators~~, one skilled in the art can scale the modulator power level <sup>any</sup>to desired levels of power and <sup>and avoid</sup>~~or voltage without the~~ limitations of the prior art.

Thus, in the configurations described above, the present invention provides a very

15 fast high-voltage switch. There are several advantages of modulators of the present invention. For example, the modulators of the present invention can replace <sup>protective</sup>~~'crowbars'~~ in vacuum tube applications <sup>the modulators</sup>~~because they~~ can typically open and close in less than 0.5  $\mu$ S. If either instantaneous or average current through the switch rises above pre-set limits, the modulator simply opens, removing power from the load. The delay from

20 sensing of an over-current condition, such as an arc, to the opening of the switch, can be kept well below 1  $\mu$ S. Another advantage is that the 'opening' of the <sup>Series</sup>~~solid state~~ switch does not shut down power supply operation, as with most conventional crowbars. <sup>Furthermore, the</sup>~~The~~

modulators of the present invention may also be used as <sup>alternatives to conventional</sup> circuit breakers. Because these switches are both opening and closing switches, power can be substantially removed from the load when the switch is <sup>commanded to its off state</sup> ~~off, or open~~. <sup>in power distribution systems and "instantly"</sup>

When the modulator of the present invention is used as a pulse modulator, the opening and closing of the modulator is controlled by a command signal at low voltage that is applied to the primary of the transformer. The result is a stream of high power pulses into the load, each with rapid <sup>(Submicrosecond)</sup> rise and fall times, and extremely consistent pulse-to-pulse characteristics.

As described previously, consistent pulse-to-pulse characteristics and fast rise times are very desirable for many applications. Thus, because the switch design and construction <sup>can be</sup> ~~is~~ identical in both a pulsed application and as a series switch, the modulator of the present invention can be used simultaneously as a pulse modulator and as a fast fault protection disconnect system. This can significantly simplify the overall design of systems that incorporate such modulators. Because solid state modulators do not use resonant circuits, each pulse can be arbitrarily sized. This allows complete pulse width and separation flexibility from 30nS to DC.

Accordingly, in another aspect, the invention features a modulator capable of switching power to meet rigorous pulse width agility requirements. In this aspect of the invention, the modulator is retriggerable. Fig. 7 is a simplified schematic of a retriggerable modulator 10, in accordance with an embodiment of the invention. This modulator includes a transformer 16, a plurality of retriggerable drive circuits 28, and a plurality of switches 18.

The transformer 16 is configured as described previously in connection with Figs.

1 through 4. Each retriggerable drive circuit 28 is electrically connected with a respective one of the plurality of secondary windings. Each switch 18 has <sup>output - high</sup> ~~input~~ and output - low terminals and a control terminal <sup>pair</sup> and is associated with a respective retriggerable drive circuit 18. The control terminal <sup>pair</sup> of each switch 18 is electrically connected with the output <sup>pair</sup> of the respective retriggerable drive circuit 28.

During operation, when a first control signal is applied to the primary of transformer 16 via the input <sup>9</sup> ~~12~~, a voltage is induced in each secondary of the transformer 16. Then, each of the plurality of switches 18 is substantially simultaneously switched by the first signal applied to the primary and remains substantially on until a second signal is applied to the primary of the transformer 16. During this time, each switch 18 can switch the power from power supply 21.

<sup>Ideally, once</sup> ~~Once~~ a switch 18 is switched on, it is not necessary to hold it in the "on" position once switching is complete. Because the input of the switch looks like a capacitor to the secondary of the transformer 18, large drive currents are only necessary to charge this capacitance quickly, but no drive current is necessary to sustain it. Thus, in theory, the <sup>primary</sup> ~~gate~~ pulse can be turned off, and the switch 18 will remain on <sup>(if the gate is isolated by a diode)</sup> until a negative pulse is provided. In practice, however, the transformer flux will reset, pulling the gate on the control input of the switch 18 negative by a small amount and shutting down the switch 18. In addition, the gate capacitance of the switch 18 is accompanied by a finite leakage, which will eventually increase the "on" state conduction losses and finally shut down the



pulse. Both of these problems can be overcome by using the retriggerable drive circuit 28 of ~~Fig. 7.~~ <sup>Figs. 7 and 8.</sup>

In operation, a gate pulse, such as a positive going pulse, passes transparently through the series FET and Zener diode of each of the retriggerable drive circuits 28, so each of the switches 18 will be switched on substantially simultaneously. When the gate pulse ends ~~or the core of transformer 16 saturates~~ <sup>however</sup> ~~However~~, the <sup>core</sup> reset voltage is insufficient to conduct through the series Zener (which has a blocking voltage of about 5V) of the retriggerable drive circuit 28. Therefore, the series FET of the retriggerable drive circuit 28 blocks the reverse bias during reset. In this manner, each switch 18

remains on either until a negative-going "end of pulse" trigger is sent through the primary, or until the gate charge leaks away. *The gate leakage can be mitigated by simply retriggering a short on pulse to keep the switch on indefinitely.*

~~Fig. 8 illustrates an alternate embodiment of the retriggerable switch. The retriggerable switch of Fig. 8 includes a bipolar voltage limiting means electrically connected in series with a gate circuit, such as back-to-back Zener diodes. In this circuit, the series FET is not required, and the gate is kept at negative voltage in the off-state for better noise immunity. This circuit requires a larger drive voltage, which also improves noise immunity.~~

In another embodiment, a <sup>refresh</sup> control circuit (not shown) can be used to generate "retrigger" pulses at specified intervals, thus recharging the control input of each switch 18 and extending the high voltage <sup>on-states and off-states</sup> pulse as long as desired.

While the preferred embodiments have been shown and described, it should be understood that there is no intent to limit the invention by such disclosure, but, rather, is intended to cover all modifications and alternate constructions falling within the spirit and scope of this invention.